

$$\bar{U}_p = 2sN = \text{mean piston speed} \quad s = \text{stroke, } N = \text{revolutions/time}$$

$w_{i,g}$ = gross indicated work per cycle = indicated work considering only compression and expansion

$w_{i,n}$ = indicated net work per cycle

$P_{i,g}$ = gross indicated power, P_f = power to overcome friction + pumping losses, P_b = net power at the crank

$$P_b = P_{i,g} - P_f = \tau\omega = 2\pi N \tau \quad \tau = \text{torque, } \omega = \text{rotational speed in rad/time}$$

$$\text{mep} = w_{\text{net}}/V_d \quad w_{\text{net}} = \text{net work per cycle, } V_d = \text{displacement volume}$$

$$\text{imep} = (\text{indicated net work})/V_d$$

$$\text{bmep} = P_b/(V_d N/n) \quad n = \text{number of crank revolutions per cycle} \quad \tau = \text{bmep } V_d/(2\pi n) \text{ so max } \tau \text{ at max bmep}$$

$$\text{fmep} = \text{friction mean effective pressure} = \text{imep} - \text{bmep}$$

$$\eta_m = P_b/P_{i,g} = \text{mechanical efficiency (Caution: Some books use } P_{i,\text{net}})$$

$$\eta_c = \text{combustion efficiency} = (\text{amount of fuel burned})/(\text{amount of fuel delivered})$$

$$\text{bsfc} = \text{brake specific fuel consumption} = \dot{m}_f/P_b$$

$$\eta_{fc} = \text{fuel conversion efficiency} = P_b/(\dot{m}_f Q_{\text{LHV}}) \quad Q_{\text{LHV}} = \text{Lower heating value of fuel used as approximation}$$

$$\eta_v = \text{volumetric efficiency} = \dot{m}_a/(\rho_a V_d N/n) \quad \rho_a \text{ can be atmospheric or intake air density, must be specified}$$

$$A/F = \dot{m}_a/\dot{m}_f = 1/(F/A) \quad \phi = (F/A)_{\text{actual}}/(F/A)_{\text{stoic}} = \text{equivalence ratio} = 1/\lambda$$

$$P_b = \eta_{fc} \dot{m}_f Q_{\text{LHV}} = \dot{m}_a (F/A) \eta_{fc} Q_{\text{LHV}} = \eta_v \eta_{fc} \rho_a V_d (F/A) Q_{\text{LHV}} N/n \quad (F/A) \text{ optimized for particular operating point.}$$

$$\tau = \eta_v \eta_{fc} \rho_a V_d (F/A) Q_{\text{LHV}} / (2\pi n) \quad \text{No explicit dependence on engine speed! } \tau \text{ tracks } \eta_v.$$

$$\frac{T_0}{T} = 1 + \frac{k-1}{2} M^2 \quad \frac{P_0}{P} = \left[1 + \frac{k-1}{2} M^2\right]^{\frac{k}{k-1}} \quad \text{Ram air: } \frac{P_{b2}}{P_{b1}} = \left[1 + \frac{k-1}{2} M^2\right]^{\frac{k+1}{2(k-1)}} \quad \text{where } P_b = \text{power}$$

$$\dot{m} = \rho \bar{V} A = \frac{P_0}{\sqrt{T_0}} A M \sqrt{\frac{k}{R}} \left[1 + \frac{k-1}{2} M^2\right]^{-\frac{k+1}{2(k-1)}} = \rho_0 c_0 A \sqrt{\frac{2}{k-1} \left[\left(\frac{P}{P_0}\right)^{\frac{2}{k}} - \left(\frac{P}{P_0}\right)^{\frac{k+1}{k}}\right]} \quad \text{Zero subscripts indicate stagnation cond.}$$

$$\text{for choked flow } \dot{m} = \rho_0 c_0 A \left[\frac{k+1}{2}\right]^{-\frac{k+1}{2(k-1)}}$$

$$\frac{P_{b2}}{P_{b1}} = \frac{P_2 - P_{v2}}{P_1 - P_{v1}} \sqrt{\frac{T_1}{T_2}} \quad \text{Power correction for pressure, temperature and humidity.}$$